

CIGRE SC A3 Tutorials and Colloquium Vienna 2011

Tutorial on Fault Current Limiters

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Content

- **Introduction**
- **Fault Current Limitation**
 - Why Fault Current Limiters (FCL)?
- **State of the Art**
 - Different types of FCLs
- **Application**
- **Requirements**
- **Power System Integration Issues**
- **Examples**



Introduction

- **CIGRE WG 13.10 - „Fault Current Limiters“**
 - **Established in 1996**
 - **15 members from 9 different countries**
 - **Reports in Electra 2001 and 2003**
 - **Technical Brochure „Fault Current Limiters in Electrical Medium and High Voltage Systems“ No. 239, 2003**
 - **Work finished and WG disbanded in 2003**

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Introduction

- **CIGRE WG A3.16 - „Fault Current Limiters“**
 - **Established in 2003**
 - **11 members from 8 different countries**
 - **Report in Electra 2008**
 - **Technical Brochure “Guideline on the impacts of Fault Current Limiting Devices on Protection Systems” No. 339, 2008**
 - **Work finished and WG disbanded in 2008**

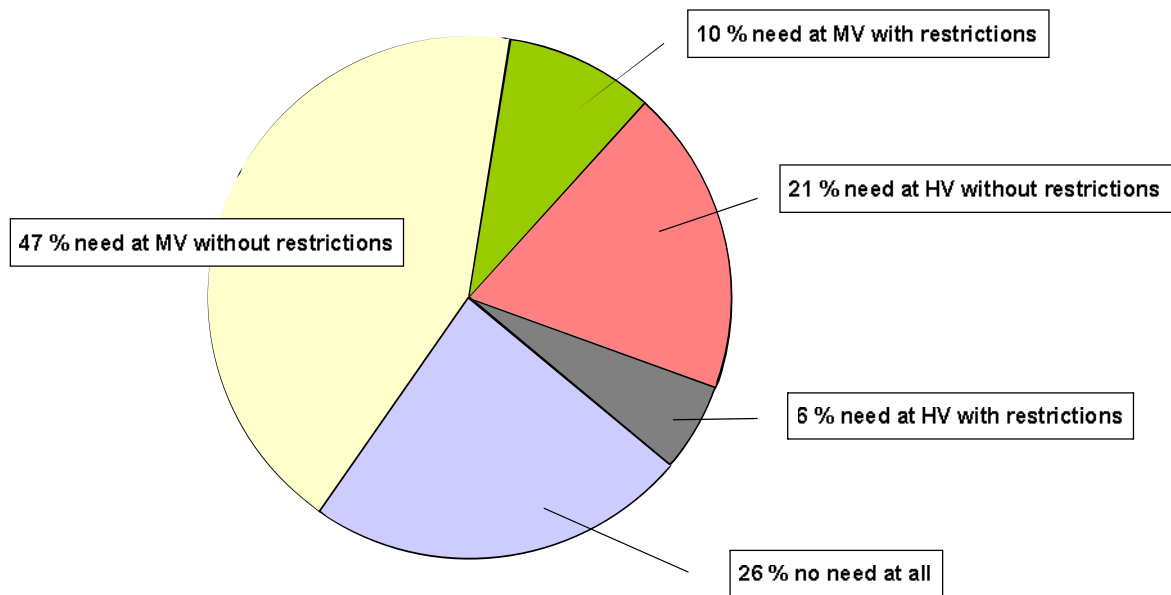
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CIGRE Questionnaire 2003 - Need for FCL



- **CIGRE WG A3.23 - „Fault Current Limiters“**
 - **Established in 2008**
 - **25 members from 11 different countries**
 - **Technical Brochure “Application and Feasibility of Fault Current Limiters in Power Systems” in process**
 - **Scheduled to finish the work in 2012**

- **CIGRE WG A3.23 – Content Technical Brochure**
 - **Fault Current Management**
 - **Past Experience and State of the Art**
 - **Application Considerations**
 - Needs and Requirements
 - Impact and Interactions
 - Reliability and Availability
 - **Feasibility and Economic Issues**
 - Case Studies
 - **Modeling Aspects**





Fault Currents: Thermal Effects



Source: Bonneville Power Administration, USA

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Fault Currents: Mechanical Effects



Source: <http://www.gaiengineers.com/photos.htm>

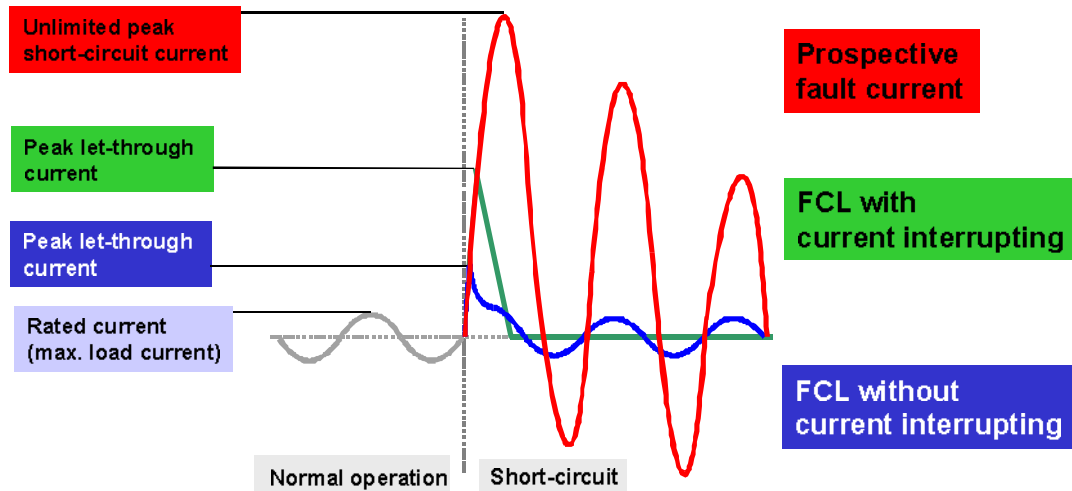
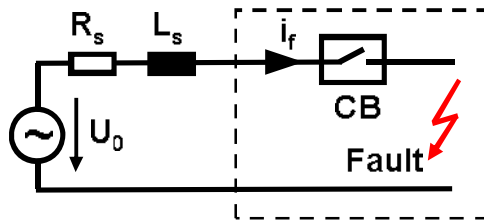
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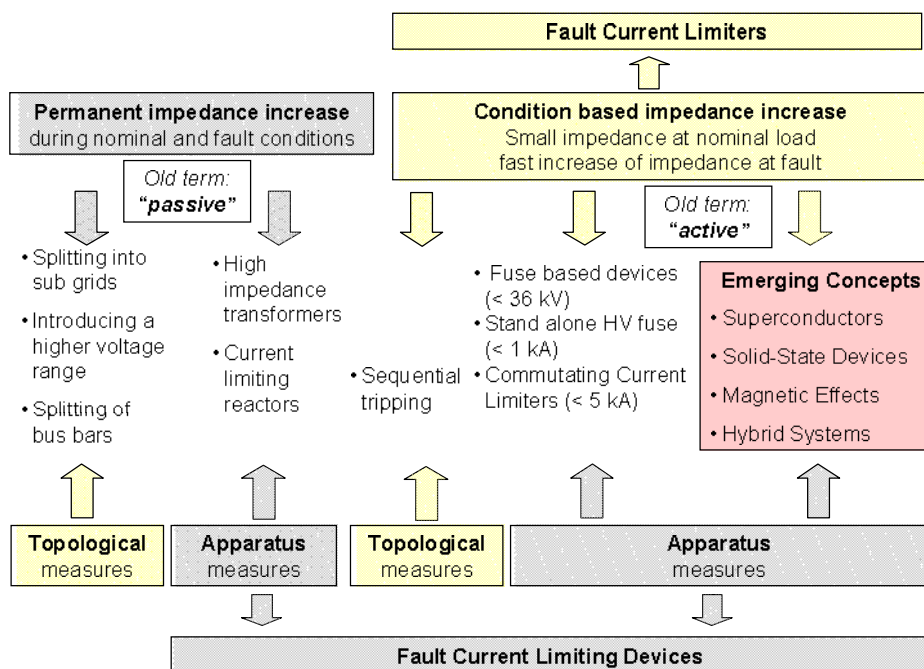
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Fault Current Limitation



Measures to Limit Short-Circuit Currents

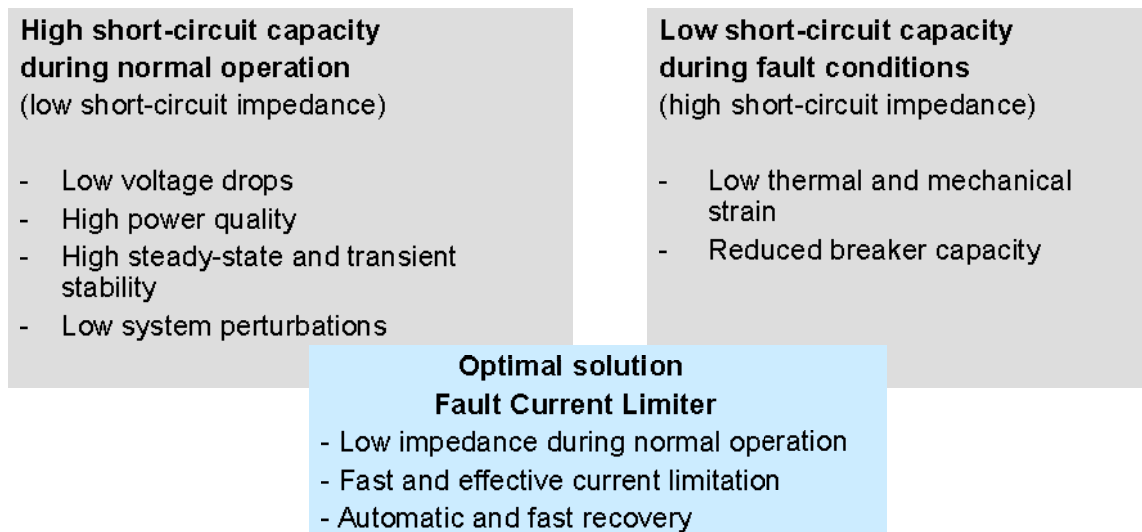


Conventional Measures to Limit Short-Circuit Currents

		Low Voltage	Medium Voltage	High Voltage
Topological measures	Introduction of a higher voltage level	applied	applied	applied
	Splitting of busbars	no	applied	applied
	Choose or upgrade to higher voltage	no	applied	applied
Apparatus measures	High impedance transformers	no	applied	applied
	Current limiting air coil reactors	applied	applied	applied
	Fuses	applied	applied	no
	Pyrotechnic Fault Current Limiter	no	applied	no

Why Fault Current Limiters ?

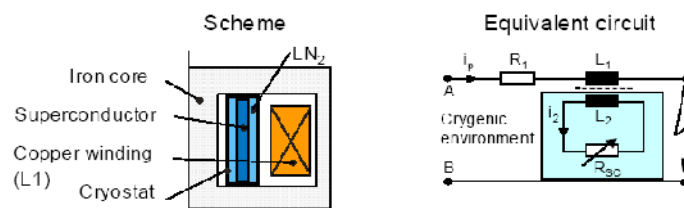
Compromise in power systems



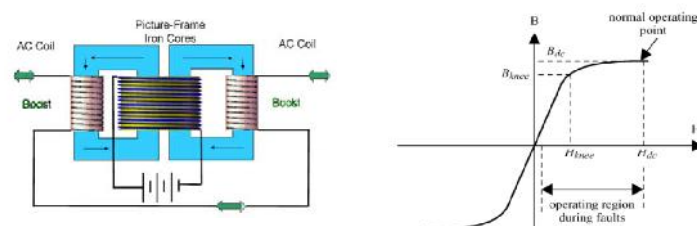
- **Conventional Devices**
 - Reactor
 - Transformer
 - Pyrotechnic Fault Current Limiter

- **Superconducting Fault Current Limiters**
 - Shielded Core
 - Saturable Core
 - Resistive FCL

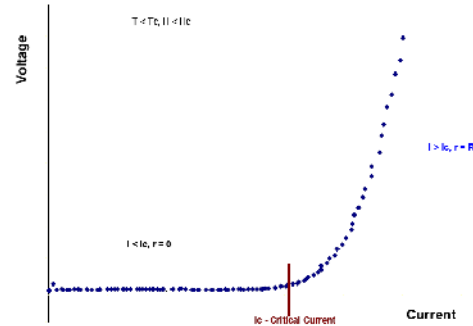
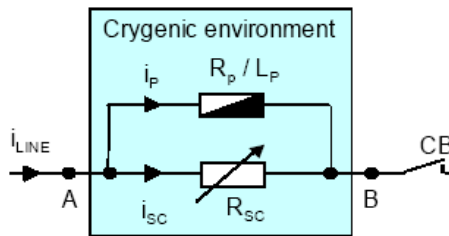
- **Shielded Core**



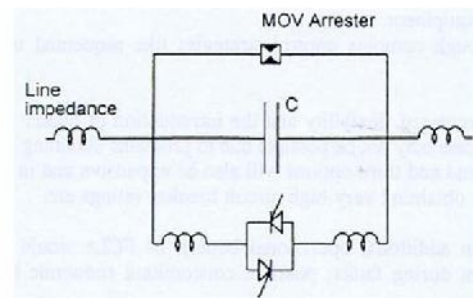
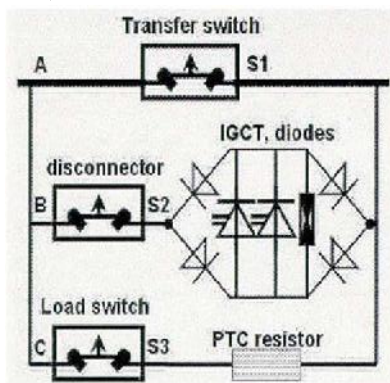
- **Saturable Core**



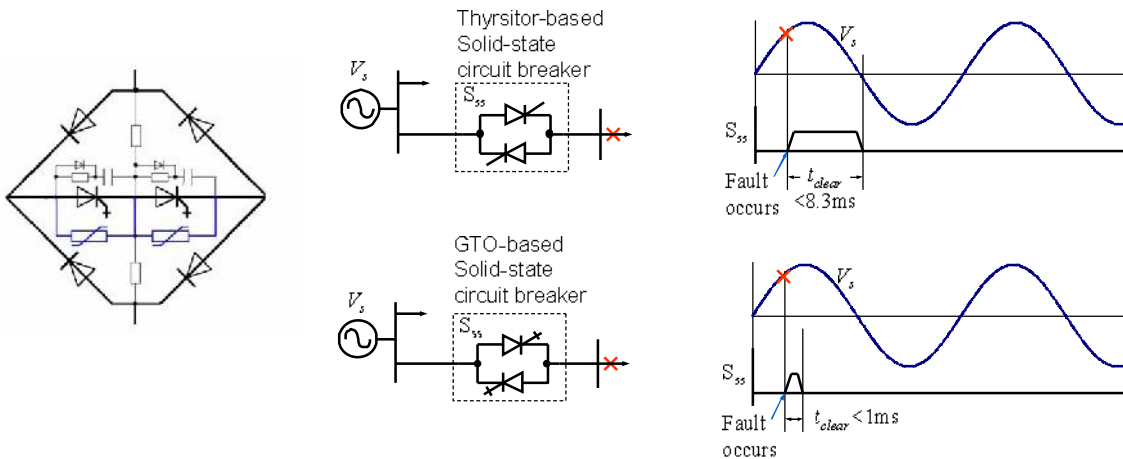
- **Resistive FCL**



- **Hybrid Systems using fast mechanical switches**
- **Polymer PTC**
- **Resonance Link (Series Compensation)**
- **Driven Arc (“LV-CB concept”)**



- **Electronic Limiters (Solid State Breaker)**
 - ➔ **Thyristor Technology**
 - ➔ **Self Commutated Device Technology (GTO, IGCT, IGBT) possible**

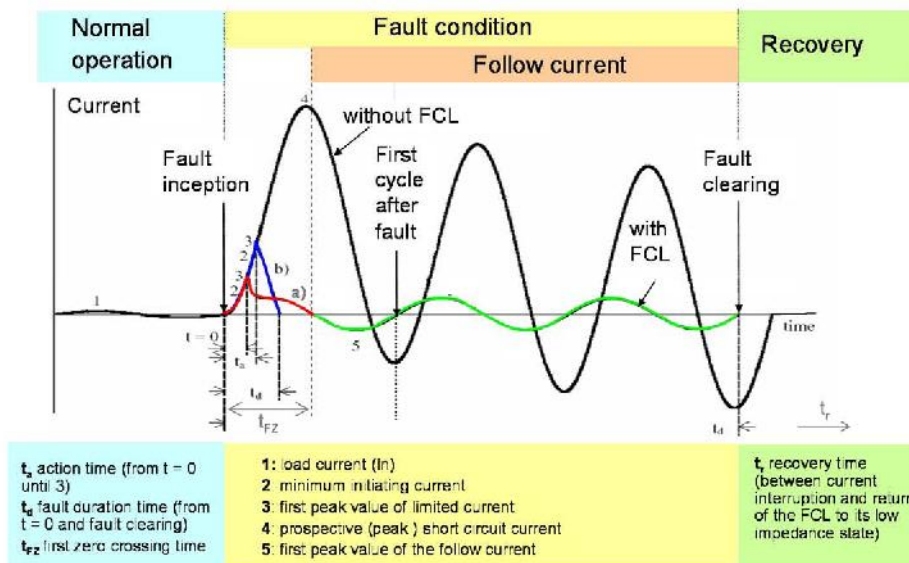


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- **Characterisation**

- **„Passive“ Fault Current Limiting Measures**

- Passive: Increase of Impedance at Nominal and Fault Conditions
(Example: Fault Current Limiting Reactor)

- **„Active“ Fault Current Limiters**

- Active: Fast Increase of Source Impedance at Fault Conditions
(Example: Superconducting Fault Current Limiter)
 - With or without Current Interruption
 - Self-triggered or External-triggered
 - „Resettable“ or „Non-resettable“ *)

*) Parts of the fault current limiter need to be replaced after an operation

Type	Passive / Active	Triggering Method	Current Interruption	Resettable	Voltage Level
Fault Current Limiting Reactor	Passive	----	---	---	MV, HV
Transformer with Increased Short-Circuit Impedance	Passive	----	---	---	MV, HV
Current Limiting Fuse	Active	Self	Yes	No	MV
Pyrotechnic Fault Current Limiter	Active	External	Yes	No	MV
Resonance Link (Kalkner Kupplung)	Active	Self	No	Yes	MV, HV

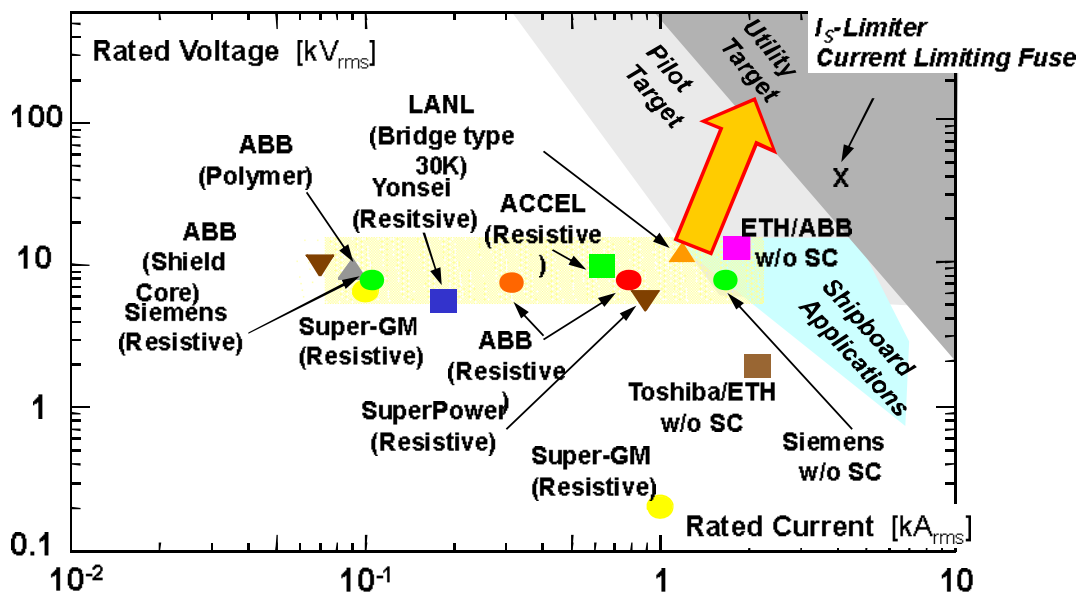
Novel Approaches

Type	Characteristics				Proto-type
	Passive/Active	Triggering Method	Current Interruption	Resettable	
Resistive Type SCFCL	Active	Self	No	Yes	MV
Shielded Iron Core Type SCFCL	Active	Self	No	Yes	MV
Saturated Iron Core Type SCFCL	Active	Self	No	Yes	MV
“Current Controller” Type SCFCL	Active	External	Yes/No	Yes	MV
FCL with PTC Resistors	Active	Self	(Yes)	(Yes)	MV
Liquid Metal FCL	Active	Self	No	Yes	MV
Current Limiting Solid-State Switch	Active	External	Yes	Yes	MV
Solid-State Switch with Current Limiting Impedance	Active	External	Yes	Yes	MV
Hybrid FCL with Solid-State Switch	Active	External	Yes	Yes	MV
Current Limiting Circuit-Breaker (with High Arc-Voltage)	Active	External	Yes	Yes	MV
Resonance Link with Switching Device (Solid-State, Vacuum)	Active	External	No	Yes	MV

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FCL Projects (Tested)

The “big step“ needed now is towards higher distribution voltages and further on to Transmission voltage levels



Status: June 2004

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Superconducting Fault Current Limiters State-of-the-Art

Lead Company	Country / Year of test	Type	Data	Phase	Superconductor
ACCEL/NexansSC	D / 2004	Resistive	12 kV, 600 A	3-ph.✓	Bi 2212 bulk
CAS	China / 2005	Diode bridge	10.5 kV, 1.5 kA	3-ph.✓	Bi 2223 tape
CESI RICERCA	Italy / 2005	Resistive	3.2 kV, 220 A	3-ph.	Bi 2223 tape
Siemens / AMSC	D / USA / 2007	Resistive	7.5 kV, 300 A	1-ph.	YBCO tape
LSIS	Korea / 2007	Hybrid	24 kV, 630A	3-ph.	YBCO tape
Hyundai / AMSC	Korea / 2007	Resistive	13.2 kV, 630 A	1-ph.	YBCO tape
KEPRI	Korea / 2007	Res.-hybrid	22.9 kV, 630 A	3-ph.	Bi 2212 bulk
Innopower	China / 2008	DC biased iron core	35 kV, 90 MVA	3-ph.✓	Bi 2223 tape
Toshiba	Japan / 2008	Resistive	6.6 kV, 72 A	3-ph.✓	YBCO tape
Nexans SC	D / 2009	Resistive	12 kV, 100 A	3-ph.✓	Bi 2212 bulk
Zenergy Power	USA / 2009	DC biased iron core	12 kV, 1.2 kA	3-ph.✓	Bi 2223 tape
Zenergy Power	USA / 2010	DC biased iron core	12 kV, 1.2 kA	3-ph.✓	Bi 2223 tape
Nexans SC	D / 2009	Resistive	12 kV, 800 A	3-ph.✓	Bi 2212 bulk
Nexans SC	D / 2011	Resistive	12 kV, 800 A	3-ph.✓	YBCO tape
Innopower	China / 2010	DC biased iron core	220 kV, 300 MVA	3-ph.✓	Bi 2223 tape
ERSE	I / 2010	Resistive	9 kV, 250 A	3-ph.✓	Bi 2223 tape
ERSE	I / 2010	Resistive	9 kV, 1 kA	3-ph.✓	YBCO tape
KEPRI	Korea / 2010	Resistive	22.9 kV, 3 kA	3-ph.✓	YBCO tape
AMSC / Siemens	USA / D / 2012	Resistive	66 kV, 1.2 kA	1-ph.	YBCO tape
Zenergy Power	USA / 2012	DC biased iron core	138 kV	3-ph. ✓	Bi 2223 tape
Nexans SC	EU / 2012	Resistive	24 kV, 1005 A	3-ph. ✓	YBCO tape

Source: M. Noe, KIT, ASC 2010



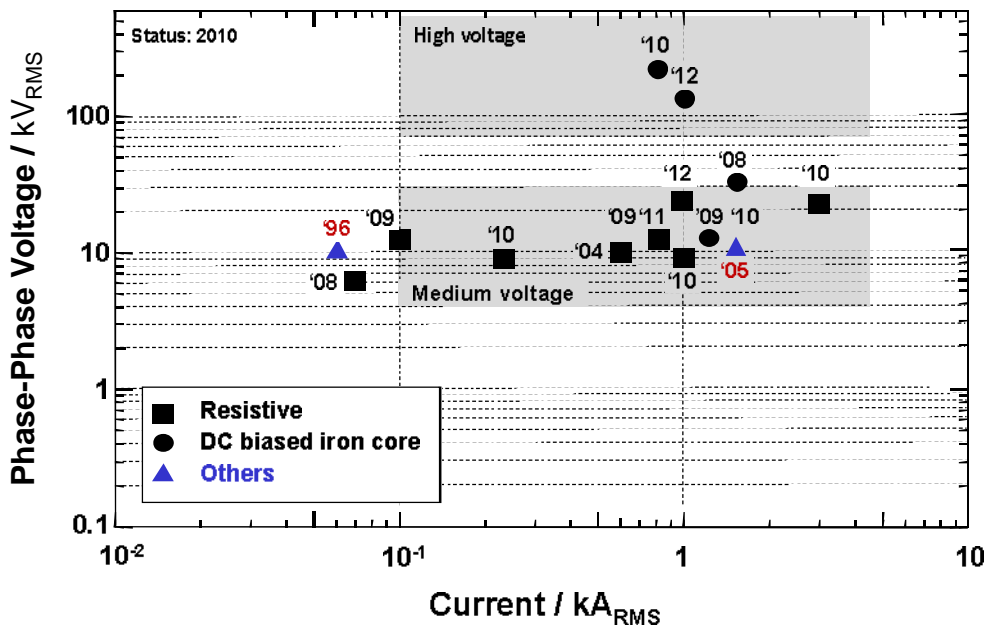
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Superconducting Fault Current Limiters SCFCL Field Tests – planned and carried out



Source: M. Noe, KIT, ASC 2010



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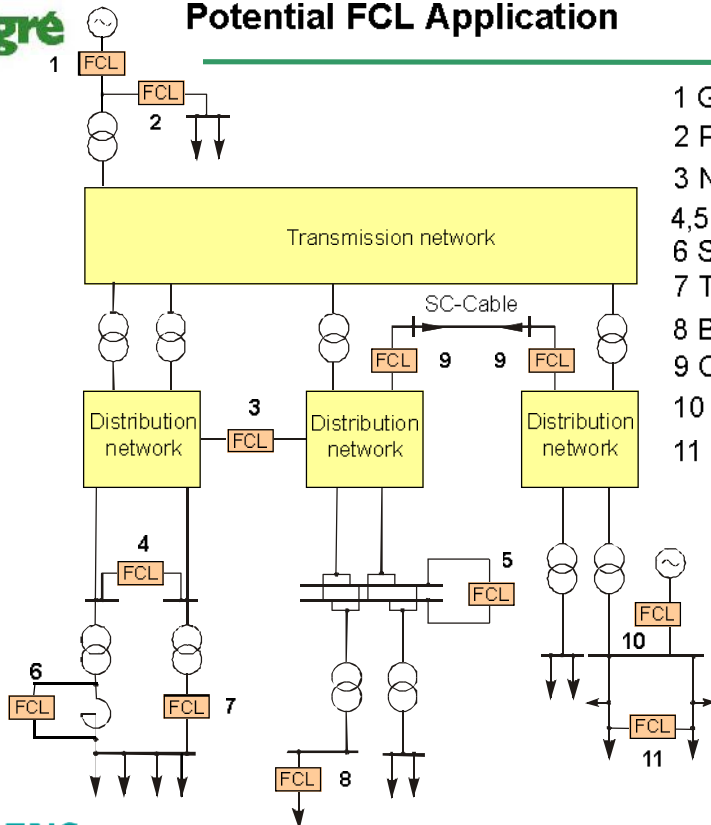
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Potential FCL Application



- 1 Generator feeder
- 2 Power station auxiliaries
- 3 Network coupling
- 4,5 Busbar coupling
- 6 Shunting current limiting reactor
- 7 Transformer feeder
- 8 Busbar connection / feeder
- 9 Combination with other SC devices
- 10 Coupling local generating units
- 11 Closing ring circuits

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Source
Noe, M.; Oswald, B.R., "Technical and economical benefits of superconducting fault current limiters in power systems", IEEE Trans. Appl. Supercon. Vol. 9/2, June 1999, pp. 1347-1350

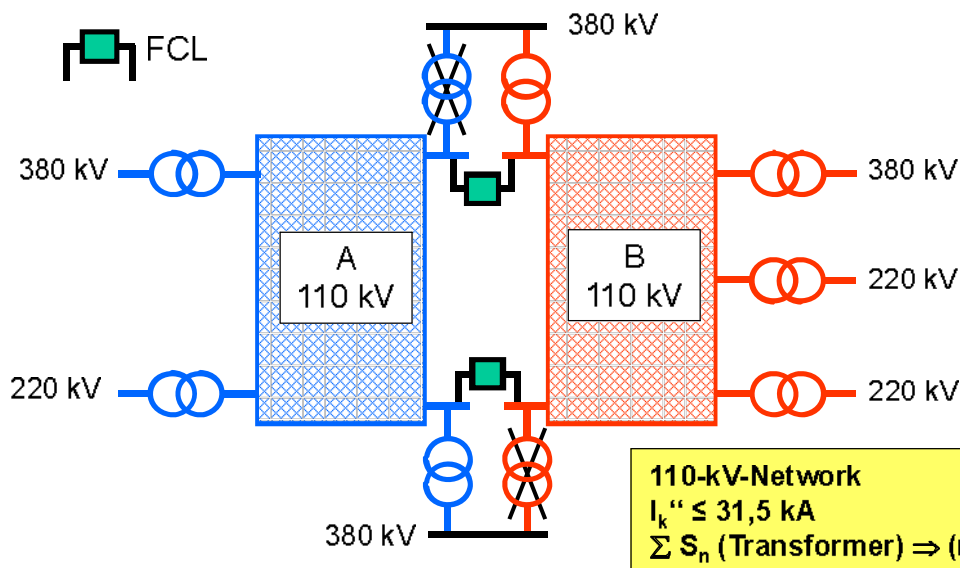
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Potential FCL Application

RWE, Germany 110 kV FCL application
Coupling of 110 kV subgrids



110-kV-Network
 $I_k'' \leq 31,5 \text{ kA}$
 $\sum S_n (\text{Transformer}) \Rightarrow (n-1)\text{-Criteria}$

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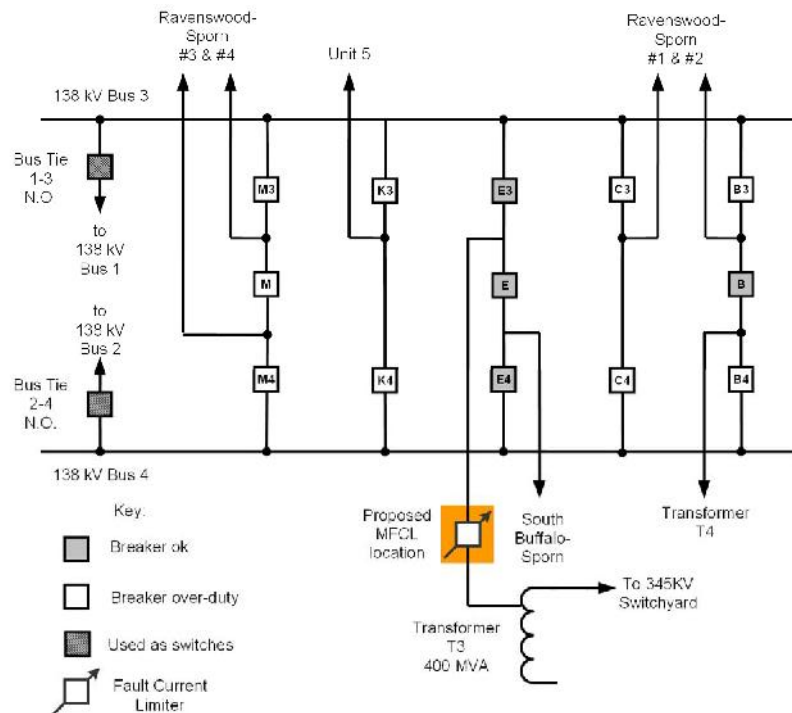


Potential FCL Application

American Electric Power (AEP) 138 kV FCL application

Reducing fault contribution from transformer feeder

Sequential tripping used to cope with high fault currents on nine existing breakers:
E3 and E trip first if fault on line #1 to #4 generator unit 5



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Advantages of the Use of FCLs

	Bus Tie	Incoming Feeder	Outgoing Feeder
Reduction of the Short-Circuit Current of the System	applied	applied	applied
Reduction of the Short-Circuit Current of the Feeder	no	no	applied
Reduction of Voltage Sags and Flicker	applied	applied	applied
Reduction of Harmonics	applied	applied	applied
Higher System Availability	applied	applied	no
Higher Loads in Sub-Systems	applied	no	no
Even Loading of Transformers	applied	applied	no



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Requirements for FCL

- **Low impedance during normal operation (low voltage drop across device)**
- **Adequate current limiting performance**
- **No deterioration of limiting behaviour during the useful life**
- **Low losses**
- **Low cost, cost effective operation**
- **Compact size and low weight**
- **No risk for operating personnel**
- **Low impact on the environment**

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Requirements for FCL

- **Technical aspects (rating)**
- **Rapid and fail safe**
- **Automatic recovery within short recovery time**
- **No excess over voltage due to current limitation**
- **No action due to transient phenomena (motor startup, capacitor energization, etc.)**
- **Integration into existing installations**
- **Compatible with existing protection system**
- **Low maintenance requirements**
- **High reliability**

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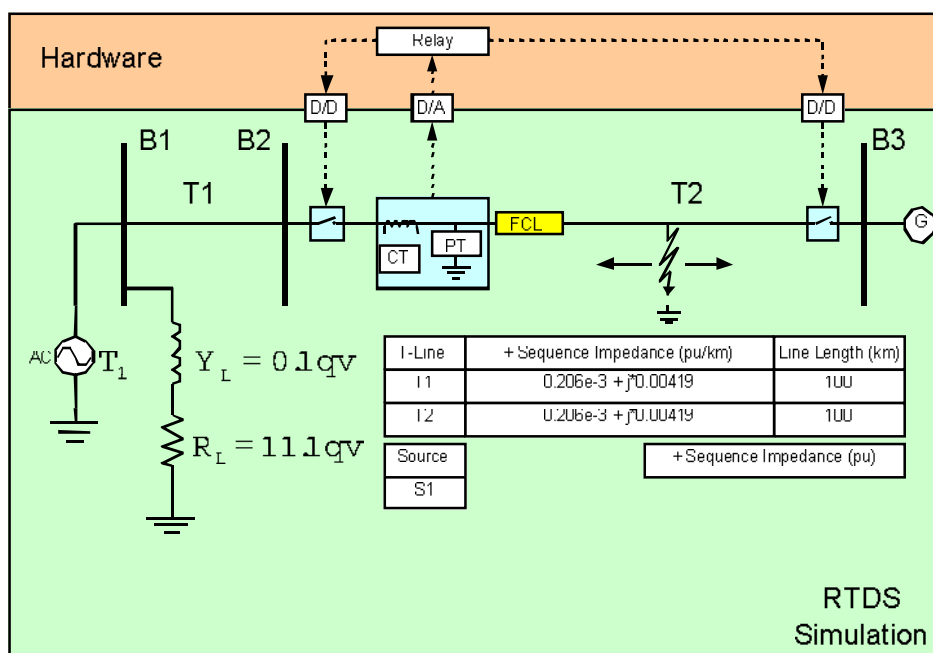
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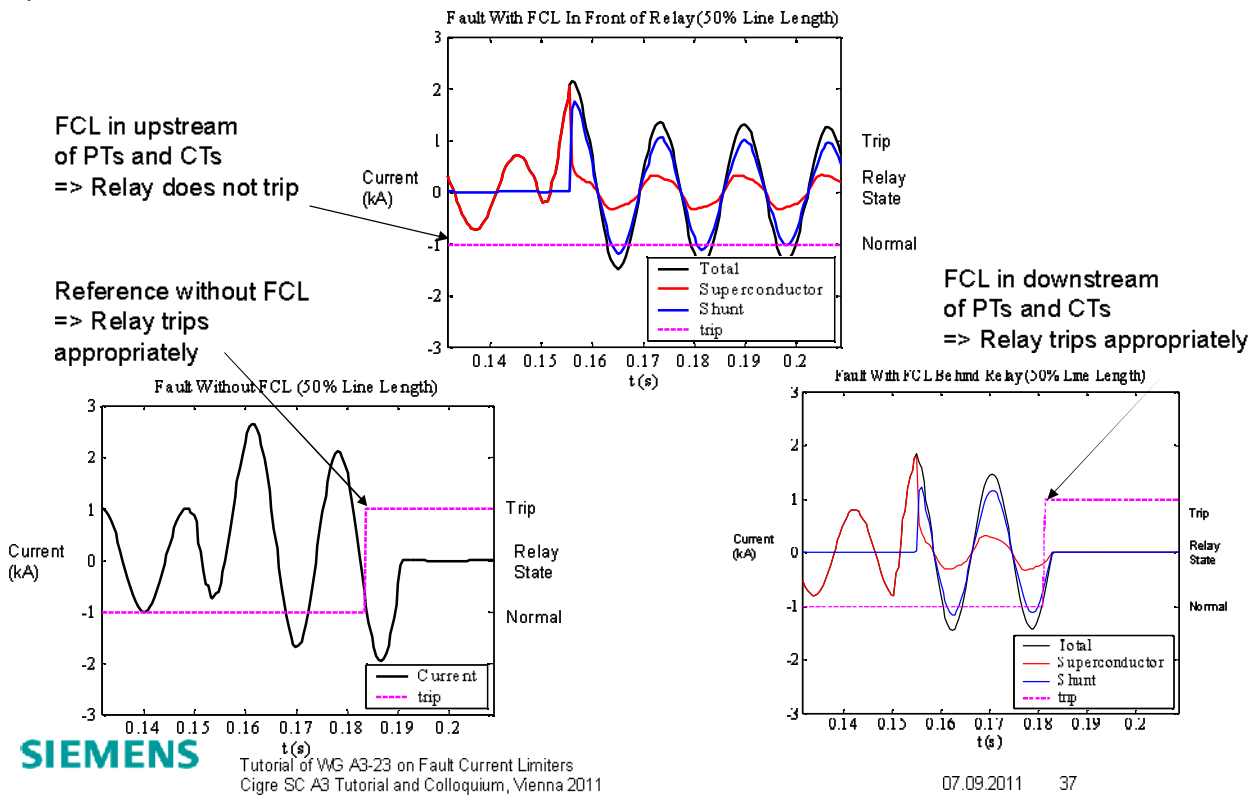
- **Effects of the System on a Fault Current Limiter**
 - **Undesirable Tripping of Fault Current Limiters**
 - Transient Currents Due to Single Phase-to-Earth Faults
 - Inrush Currents Due to Transformer Switching
 - Inrush Currents Due to Capacitor Bank Switching
 - Starting Currents of Motors
 - **Ability of Fault Current Limiters to Withstand Fault Currents**
 - **Fault Duration Depending on Protection System**

- **Effects of a Fault Current Limiter on the System**
 - **Effects on System Reliability**
 - Reliability of the Fault Current Limiter
 - Effect of a Malfunction of the Fault Current Limiter
 - Behaviour of the Fault Current Limiter in Case of an Internal Fault
 - **Maintenance Requirements**
 - Maintenance Intervals
 - Maintenance Duration

- **Effects of a Fault Current Limiter on the System**
 - **Effects on Protection Schemes**
 - Relay Settings
 - Selectivity
 - Compatibility with Downstream Fuses
 - Protection Blinding (e.g. in Case of Directional Protection)
 - **Effects on Conventional Switchgear**
 - Transient Recovery Voltage of Downstream Circuit-Breakers
 - **Transient Stability**
 - Impact on Rotor Angle Stability

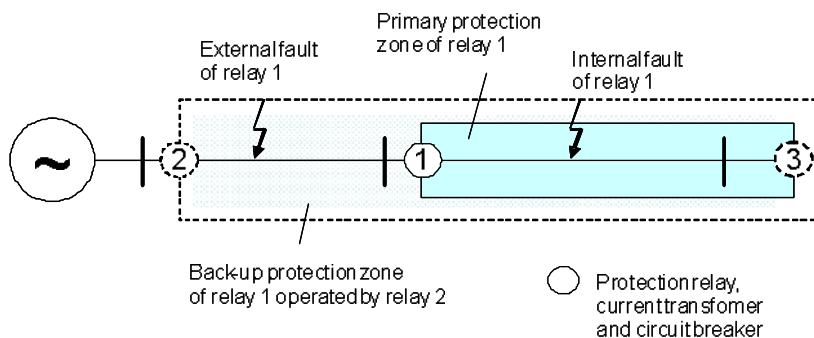


Results: FCL leads to missing trips



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Protection Zone Concept



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- **Sensing**
 - **Transmission Errors**
- **Pickup**
 - **Distinction between load and fault condition**
- **Processing**
 - **Evaluation of measured values**
- **Coordination**
 - **for selectivity protection relays must be coordinated with each other**

Protection principles	Pickup		Processing		Coordination	
	FCL Inside	FCL outside	FCL Inside	FCL outside	FCL Inside	FCL outside
Overcurrent 50/51	1 : overcurrent pickup: $I_{sc FCL} > I_{Pickup}$		6 : FCL fault duration > processing time, additionally delay due to inverse-time characteristics		12 : current grading, current blinding	13 : source-impedance ratio (SIR) – grading
Directional functionality 67	2 : zone impedance pickup (refer to 3)		6, 7, 8 : range of line phase angles including FCL, signal distortion	6, 8, 9 : determination of direction based on source impedance	No coordination, because the directional stage is added to overcurrent or distance function	
Distance 21	1, 3 : overcurrent pickup, impedance pickup $Z_{Fault} < Z_{Pickup}$	1 : overcurrent pickup, no influence on impedance pickup	3b, 6, 8 : zone impedance sensing	6, 8, 9 : determination of direction based on source impedance	14 : Inter-in-feed effect	15 : source-impedance ratio (SIR) - accuracy
Differential 87 - Low impedance	1, 4 : Overcurrent pickup or overcurrent guarding		6, 10 : lower fault current, check for sensitivity		16 : No coordination with other types of protection, only some unusual exceptions	
Differential 87 - High impedance	5 : No overcurrent pickup facility, differential current measurement only		6, 11 : lower fault current, check for sensitivity			

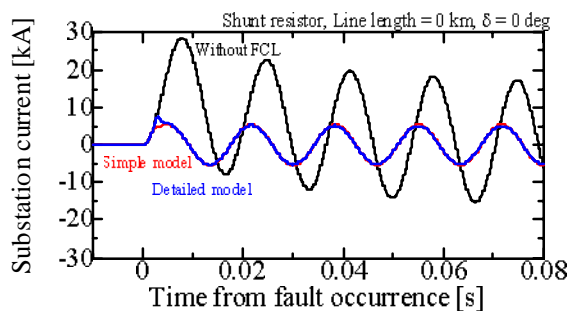
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- No adverse influence as long as the minimum limited fault current measured by the relay, depending on the limitation factor and possible current distortion of the FCL, still exceeds the threshold for pickup current of the overcurrent function.

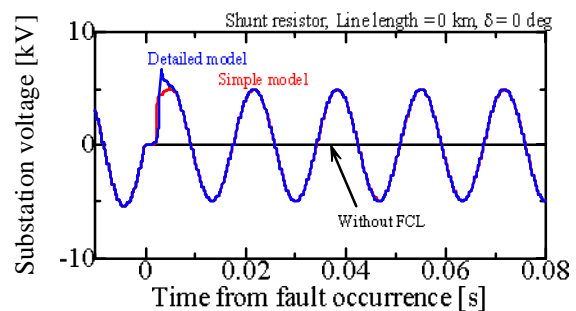
6:

- The FCL must allow the fault current to flow at least as long as the sum of all processing times and the delay times. This depends on the fault duration time of the FCL.

	Detailed model	Simple model
HTS resistance	E-J characteristic HTS temperature	Linear model
Resistance of shunt resistor	Constant	Constant
Inductance of shunt coil	Constant	Constant
Resistance of shunt coil	Depend on temperature	Constant



(a) Substation current



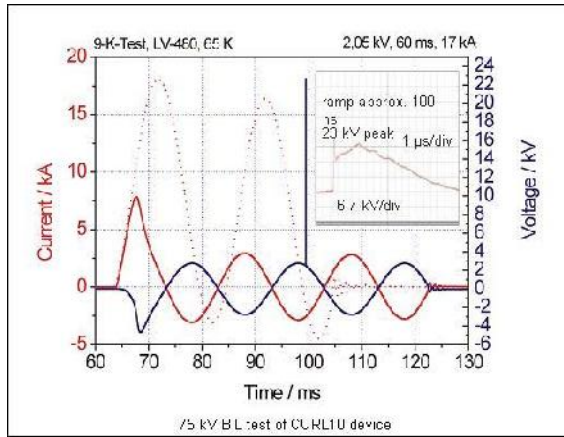
(b) Substation voltage

- **Existing Standards:**
 - ➔ **Fault Current Limiting Reactors (IEC 60289)**
 - ➔ **High Voltage Fuses (IEC 60282-1)**
 - ➔ **Power Transformers (IEC 60076)**

- **For all other Types of Fault Current Limiters no Standards Exist**

No.	Type	Existing IEC Standard
1	Winding resistance	IEC 60076-6
2	Impedance	IEC 60076-6
3	Total losses	IEC 60076-6
4	Temperature rise	IEC 60076-6, IEC 60076-2
5	Applied voltage	IEC 60076-6
6	Insulation power factor	IEC 60076-11
7	Insulation resistance	IEC 60076-11
8	Turn to turn	IEC 60076-11, IEC 60076-3
9	Lightning impulse	IEC 60076-11, IEC 60076-3, IEC 60076-4
10	Chopped wave	IEC 60076-11, IEC 60076-3, IEC 60076-4
11	Partial discharge	IEC 60076-3, IEC 60076-6,
12	Seismic verification via analysis	A new IEC standard will be created, actually IEEE Standard 693 is used

Standard FCL Testing Procedures Needed



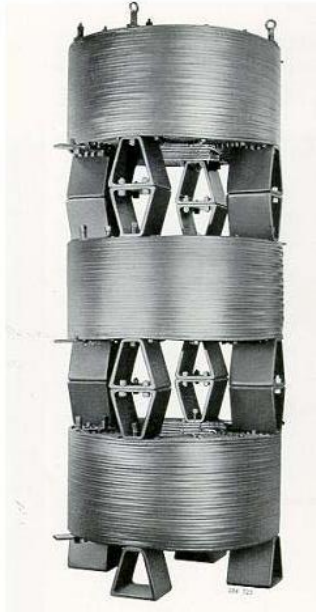
75 kV BIL test of CURL10 device

- In the past: Individual requirements defined by host utility
- Voltage impulse test for FCL
 - All terminals to ground for FCL open
 - Terminal to Terminal one phase
 - lightning impulse during FCL action
- Short time withstand current testing
 - “Active part bridged” for FCLs which inherently do not allow the prospective fault current to flow
- “Reclosing”
 - Expected duty comparable to circuit breaker (e.g. O-C-O). Is this really required for all applications?

Power System Integration Issues with FCL

- FCL characteristics introduce new system dynamics
 - Standard testing procedures must be developed
 - System protection must be investigated
 - How to coordinate FCL characteristic with existing protection schemes?
 - New protection schemes are possible with FCL for future systems
 - Validated models for system simulation studies needed
 - New materials for FCL (e.g. Cryogenics)
 - Utilities/users are not familiar with

Limiting Reactor MV



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Limiting Reactor 110kV



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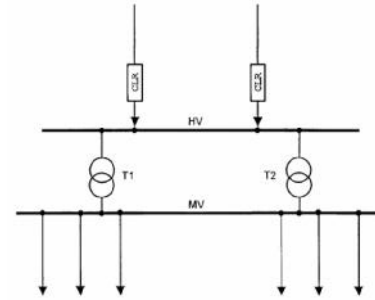
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Application of Fault Current Limiters - Examples

Limiting Reactor 362 kV



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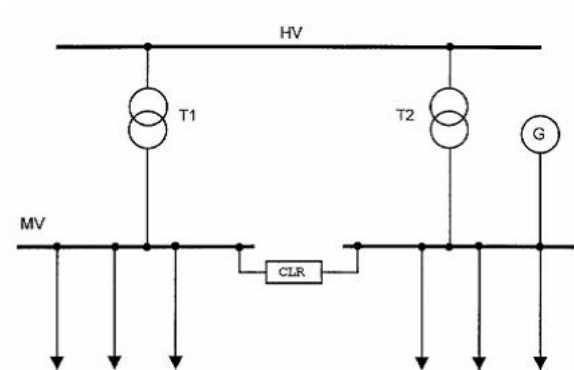
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Application of Fault Current Limiters - Examples

Limiting Reactor 550 kV



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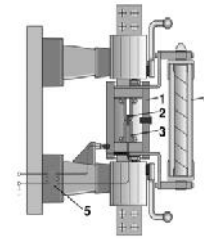
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Pyrotechnic Fault Current Limiter



Courtesy G&W



Courtesy ABB

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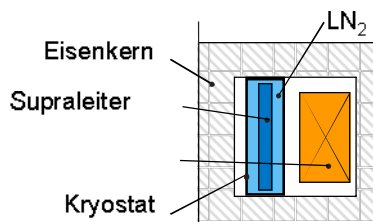
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Superconducting FCL (Inductive Type) - 1996 (abgeschirmter Eisenkern)

Schema



Daten:	
Spannung	10 kV
Strom	70 A
Temperatur	77 K
BSCCO2212 Zylinder	

Courtesy ABB

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Superconducting FCL (Resistive Type)



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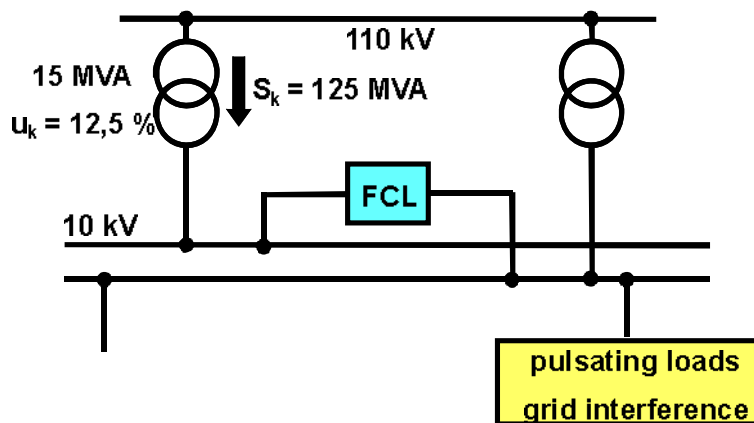
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World wide first resistive SC-FCL field test
at RWE, Germany (field test started April 2004)

Demonstrator application in a 10 kV busbar coupling



Main data:

Voltage	12 kV
Current	600 A
Lim. time	60 ms
Max. current	8.75 kA
Temperature	65 K
Max. E-field	0.6 V/cm
MCP-BSCCO2212 bifilar coils	



Photo: ACCEL, Germany

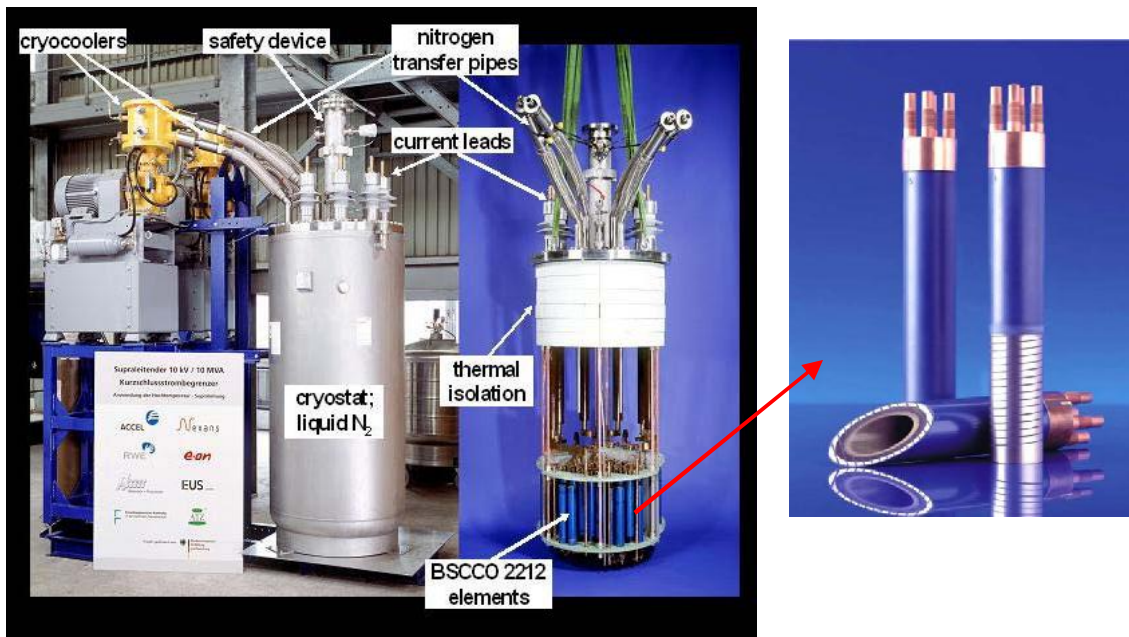
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Superconducting FCL (Resistive Type BSCCO) - 2004



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Superconducting FCL (Resistive Type YBCO) - 2008

Toshiba, Fujikura: CC Fault Current Limiter - Non-Inductive and Parallel Winding Coils by a High Resistive (@ normal state) CC-

Source: Yamada, US Doe Peer Review 2008

3-Phase Fault Current Limiter Coil

Install into cryostat with rel. (~70K, 1 atm)

High Resistive Coated Conductor for Fault Current Limiter
Target: $R > 0.1 \Omega/m$ @rt & no damage for $2 \cdot I_n \times 2ms$

Ni-Cr alloy (Ni77%, Cr20%) tape 0.1 mm-t 5 mm-w
Sn Solder Plating

Ag : 5-20mm

$I_n = 189A/5mm$ 0.19Ω/m & no damage @ 400A×3ms

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Superconducting FCL – 2009



Source: LSIS

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Electronic Limiter



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Electronic Limiter (Solid State Limiter) - 2004



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Strombegrenzer mit Diodenbrückenschaltung - 2005

Daten:

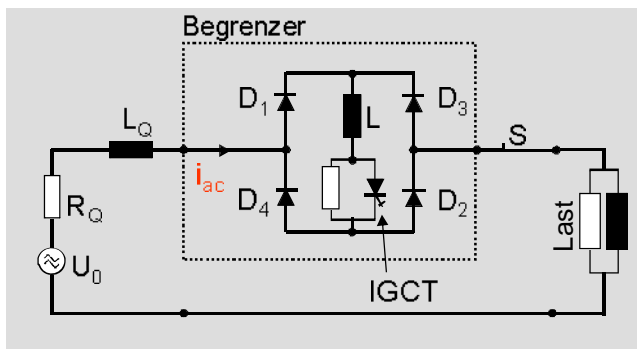
Spannung 10.5 kV

Blitzstossspannung 75 kV

Strom 1.5 kA

Spuleninduktivität 6.24 mH

Installation in der Gaoxi Schaltanlage



HTS Spule

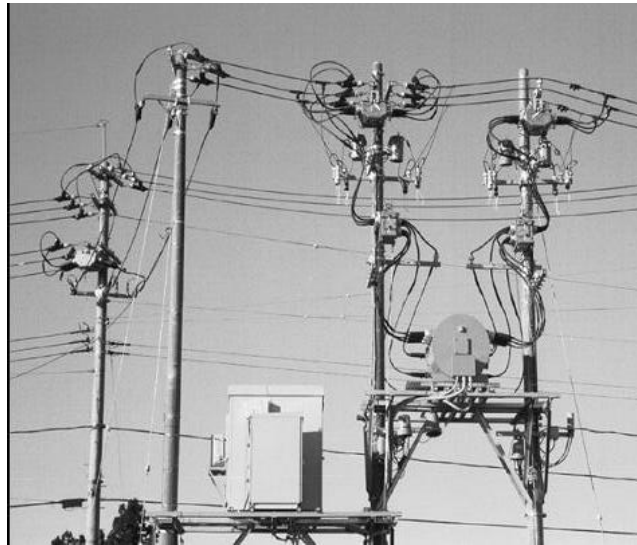
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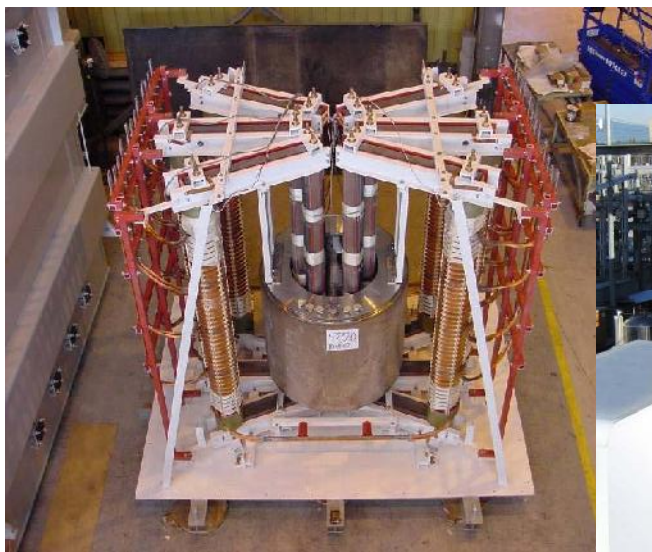
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Arc Driven FCL



Saturable Core (2009)



Prototype 13 kV



Courtesy:
Zenenergy Power

Installation in the system of Southern California Edison

Short Circuit Tests at Powertech Labs British Columbia, December 2007



Superconducting Fault Current Limiters State-of-the-Art

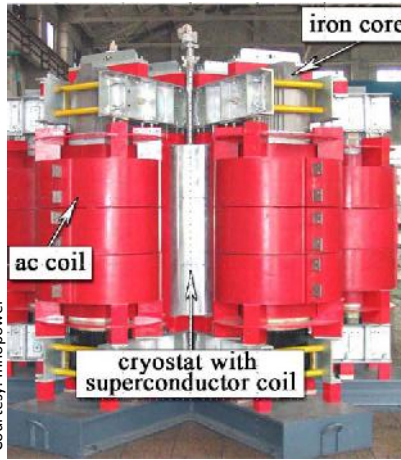
Nexans SuperConductors



Courtesy: Nexans SuperConductors

Resistive Type
12 kV, 800 A, 120 ms
Bi 2212 bulk material
Power system auxiliary
Energized 2009
First commercial system

Innopower



Courtesy: Innopower

DC Biased Iron Core Type
35 kV, 90 MVA
Bi 2223 tapes
Substation
Energized 2008

Zenergy Power



Courtesy: Zenergy Power

DC Biased Iron Core Type
15 kV, 1.2 kA, 60 cycles
Bi 2223 tapes
Substation Feeder
Energized March 9, 2009



Tutorial of WG A3-23 on Fault Current Limiters
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Source: M. Noe, KIT, ASC 2010

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63

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Thank you for your attention

Tutorial on Fault Current Limitation

The End



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